

# Effect of Rail Seat Deterioration on Rail Seat Load Distributions



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**RAILTEC**  
UNIVERSITY OF ILLINOIS AT URBANA-CHAMPAIGN

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# Outline

- Research Objectives
- Experimentation Overview
  - Wear Depth Profiles
  - Instrumentation Plan
- Rail Seat Load Distribution Data
- Rail Base Displacement Data
- Preliminary Conclusions
- Future Work



# Objectives of FRA Task Order 333

- To improve automated inspection of concrete tie rail seat deterioration (RSD)
- To further this objective additional instrumentation and data analysis was provided by UIUC
- Data collected will be incorporated into the project in order to further understand:
  - Rail movement on pre-existing RSD
  - Rail base contact with pre-existing deteriorated rail seats
- This data will augment testing from commercial suppliers of detection services and other research cars

# Objectives of UIUC Experimentation with Matrix Based Tactile Surface Sensors (MBTSS)

- Compare pressure distribution on rail seats:
  - Under various loading scenarios
  - Under presence of fines
  - Under various stages of rail seat wear
- Develop design metric for mechanistic evaluation of rail seat load distribution



# Objectives of RSD Experimentation

- Quantify effect of RSD wear shape and depth on rail seat load distribution
- Correlate rail base rotation to excessive rail seat pressure
  - Encourage mechanistically-defined inspection thresholds to detect unsafe levels of RSD
- Use relationships to guide thresholds for proposed rail seat load distribution design metric

# Rail Seat Deterioration Background

- Rail Seat Deterioration (RSD) is the degradation of concrete directly underneath the rail pad, resulting in track geometry problems
- Surveys conducted by UIUC report that North American Class I Railroads and other railway infrastructure experts ranked RSD as one of the most critical problems associated with concrete crosstie and fastening system performance
- Potential RSD mechanisms as determined through research at UIUC:
  - Abrasion
  - Crushing
  - Freeze-thaw
  - Hydraulic pressure cracking
  - Hydro-abrasive erosion

Gauge

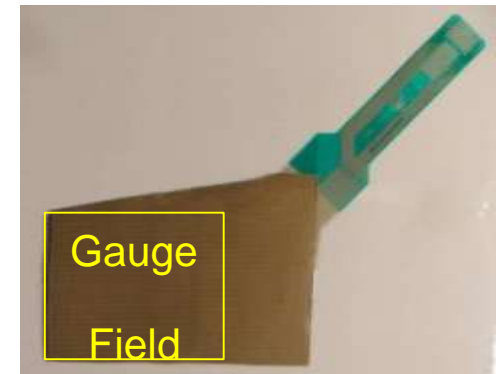
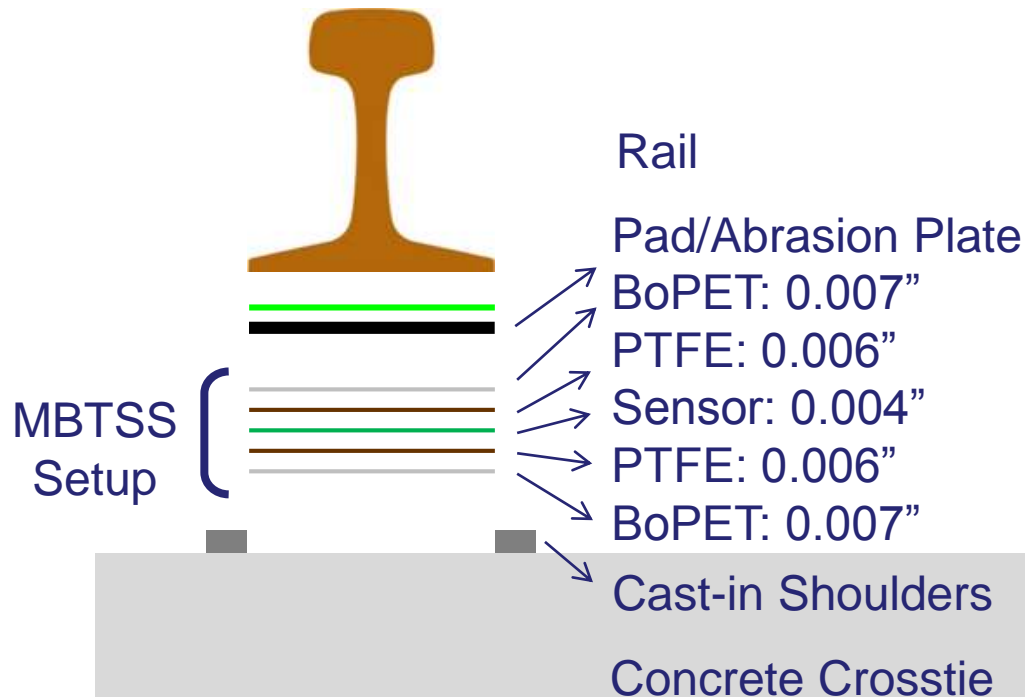


Field



# Equipment Preparation and Protection

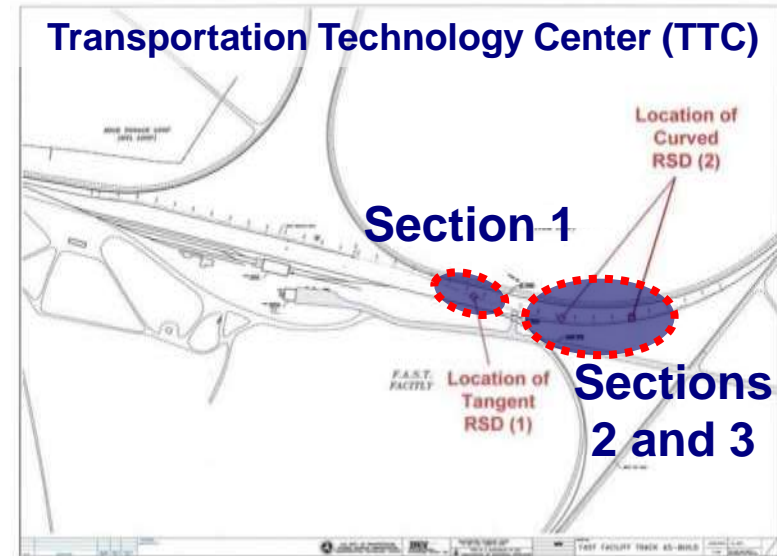
- Sensors trimmed to fit rail seat
- BoPET and PTFE layered on each side of sensor to protect from shear and puncture damage
- Plastic sleeves and plastic bags to protect sensor tabs and handles from puncture and debris



Plan View of Sensor and Protective Layers

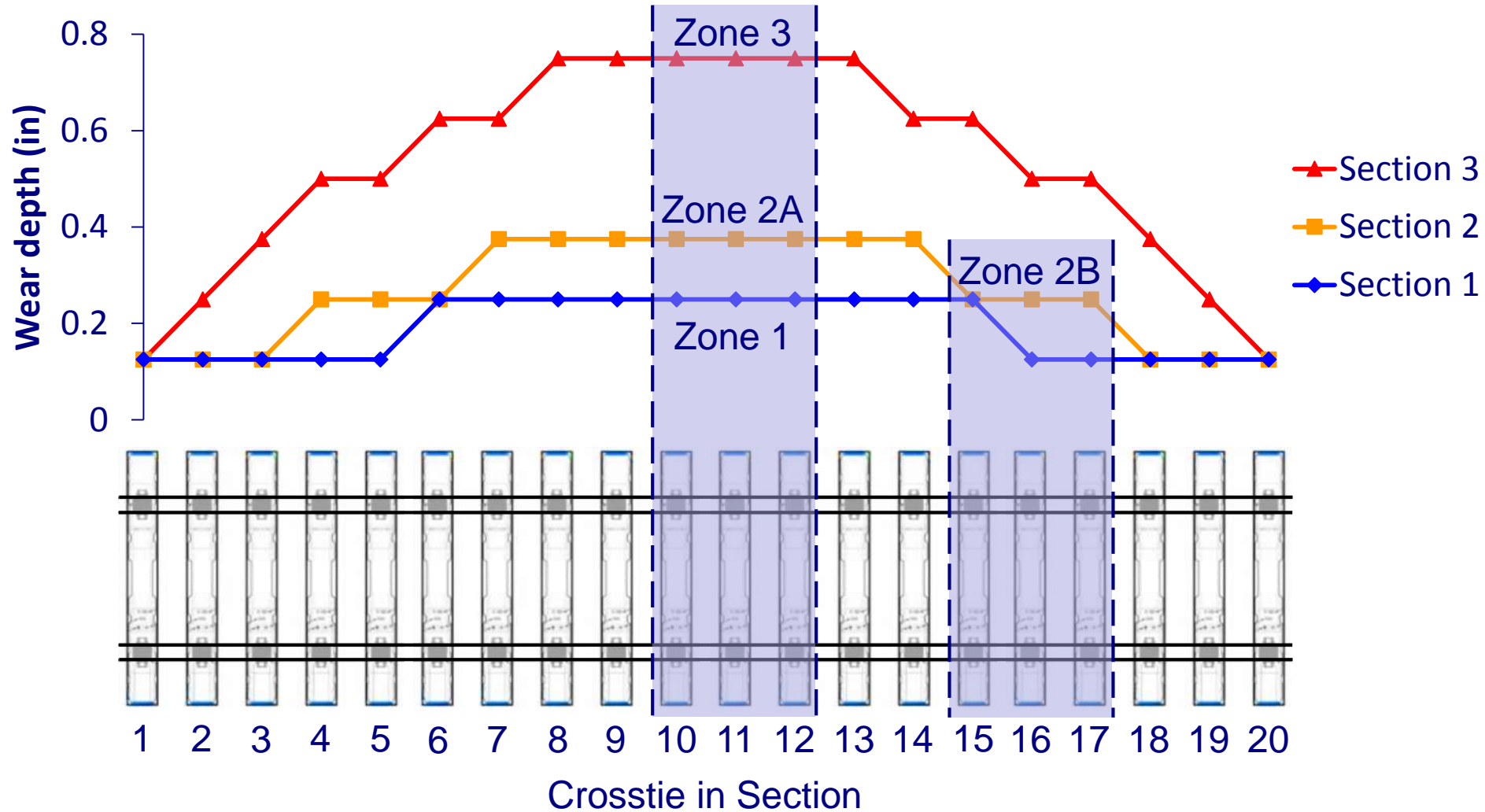
# Field Experiment Program

- **Objective:** Analyze the effect of RSD depth and shape on rail seat load distribution and correlate to rail base rotation
- **Location:** Transportation Technology Center (TTC) in Pueblo, CO
  - **Section 1:** tangent section with 1/4 inch uniform wear
  - **Sections 2 and 3:** curved sections with 1/4, 3/8, and 3/4 inch triangular wear
- **Instrumentation:**
  - MBTSS deployed to capture rail seat pressures and contact area
  - Potentiometers to capture rail base displacement
- **Loading:** FRA T-18 used to apply static and dynamic loads to the track structure
  - Gauge restraint measurement system (GRMS) used to generate varying L/V ratios

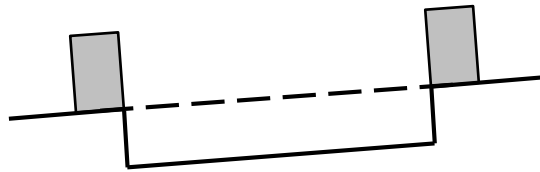




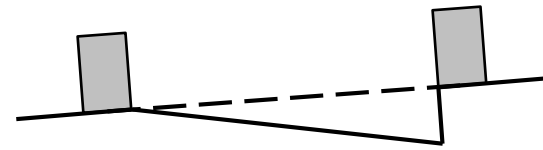
# RSD Section Wear Depths



# Rail Seat Wear Profiles



Uniform Wear (Zone 1)



Triangular Wear (Zone 2A, 2B, 3)

## Zone 1

**1/4" Uniform  
Wear**

## Zone 2B

**1/4" Triangular  
Wear**

## Zone 2A

**3/8" Triangular  
Wear**

## Zone 3

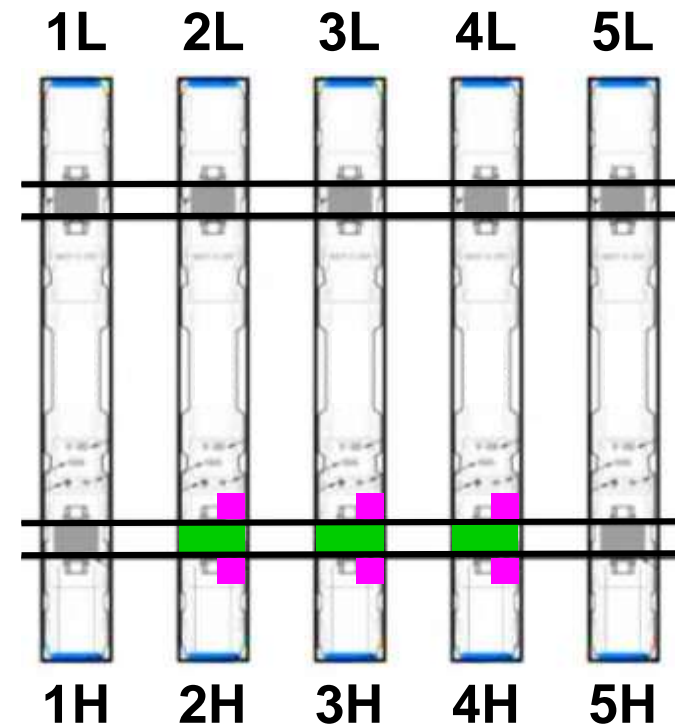
**3/4" Triangular  
Wear**



- Smooth, planar rail seat surface
- Field-worn RSD often causes exposed aggregate
  - May generate load concentrations not represented in artificially-worn rail seats

# Instrumentation Plan

- Three adjacent ground (high) rail seats instrumented
  - MBTSS used to capture rail seat pressure distribution
  - Potentiometers on rail displacement fixtures used to capture rail base vertical displacement
    - Used to calculate rail base rotation
- No unground (low) rail seats instrumented



 MBTSS

 Rail Displacement  
Fixture

# Experimental Matrix

- 20,000 lb (88.9 kN) vertical load constant for all tests
- Static tests:
  - L/V force ratios of 0 to 0.8 at 0.2 L/V intervals
  - Load applied at all 3 instrumented rail seats, as well as one rail seat on either side of instrumentation zone
- Dynamic tests:
  - L/V Force ratios of 0, 0.4, and 0.8
  - Conducted at 5 and 15 mph

# Rail Seat Load Concentration

20,000 lb (88.9 kN) Vertical Wheel Load, 0.6 L/V Force Ratio

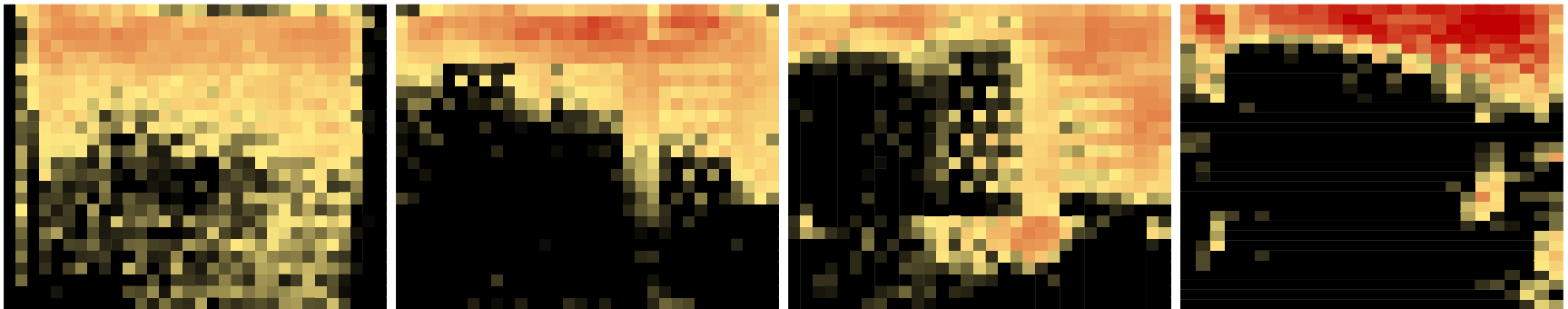
0" Wear  
(May 2013)

1/4" Triangular  
Wear

3/8" Triangular  
Wear

3/4" Triangular  
Wear

Field



Gauge

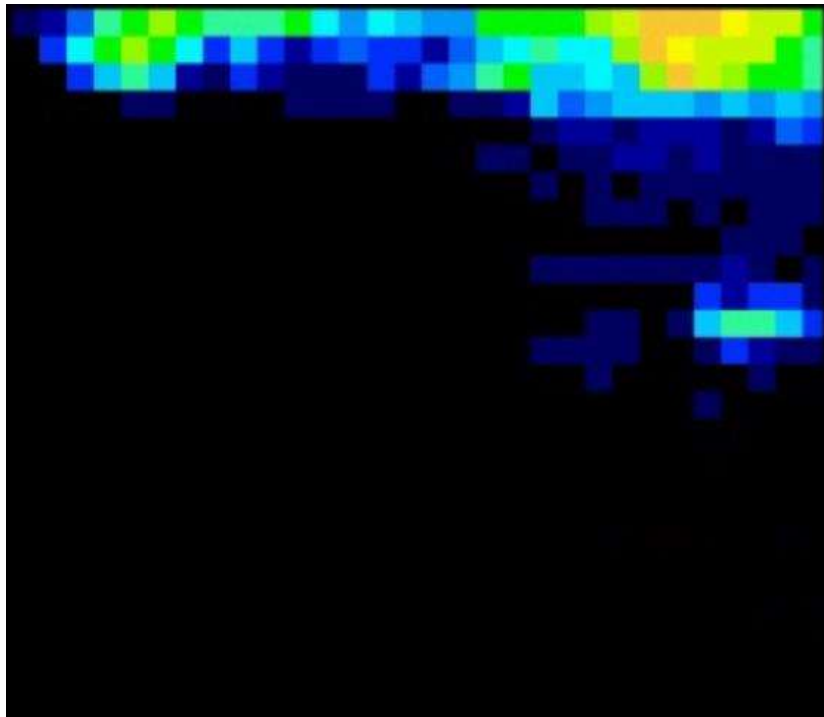
- General trend of increasing load concentration toward field side of rail seat with increased wear depth
- Trend of load concentration on right side of rail seat

# T-18 Dynamic Run

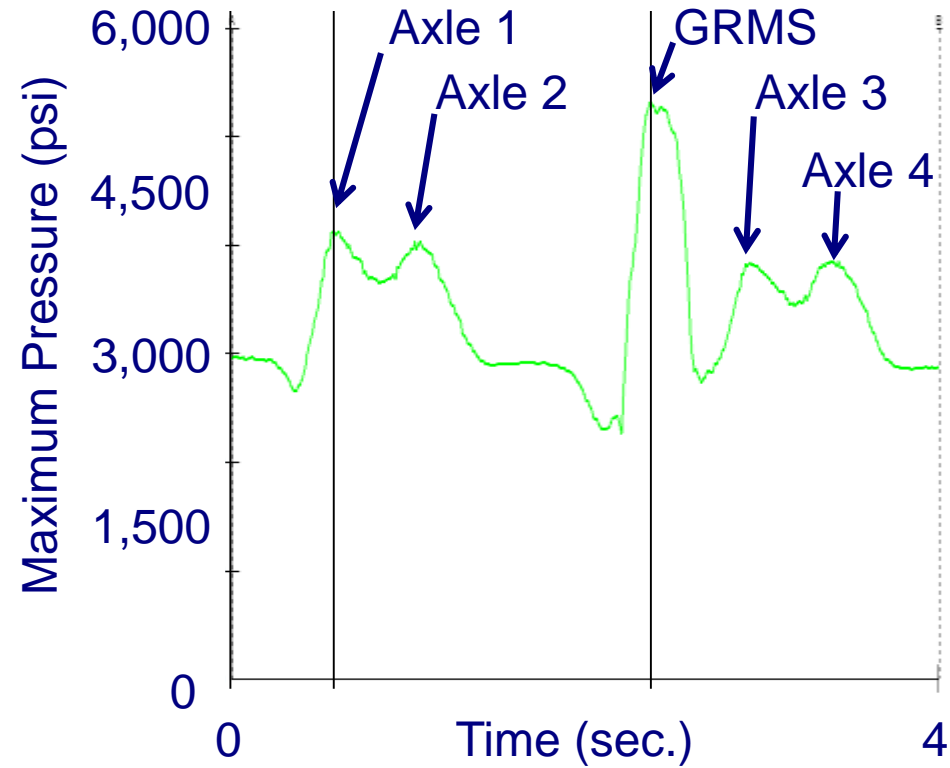
20,000 lb (88.9 kN) Vertical Wheel Load, 0.8 L/V Force Ratio

3/4" Wear, 15 mph

Field



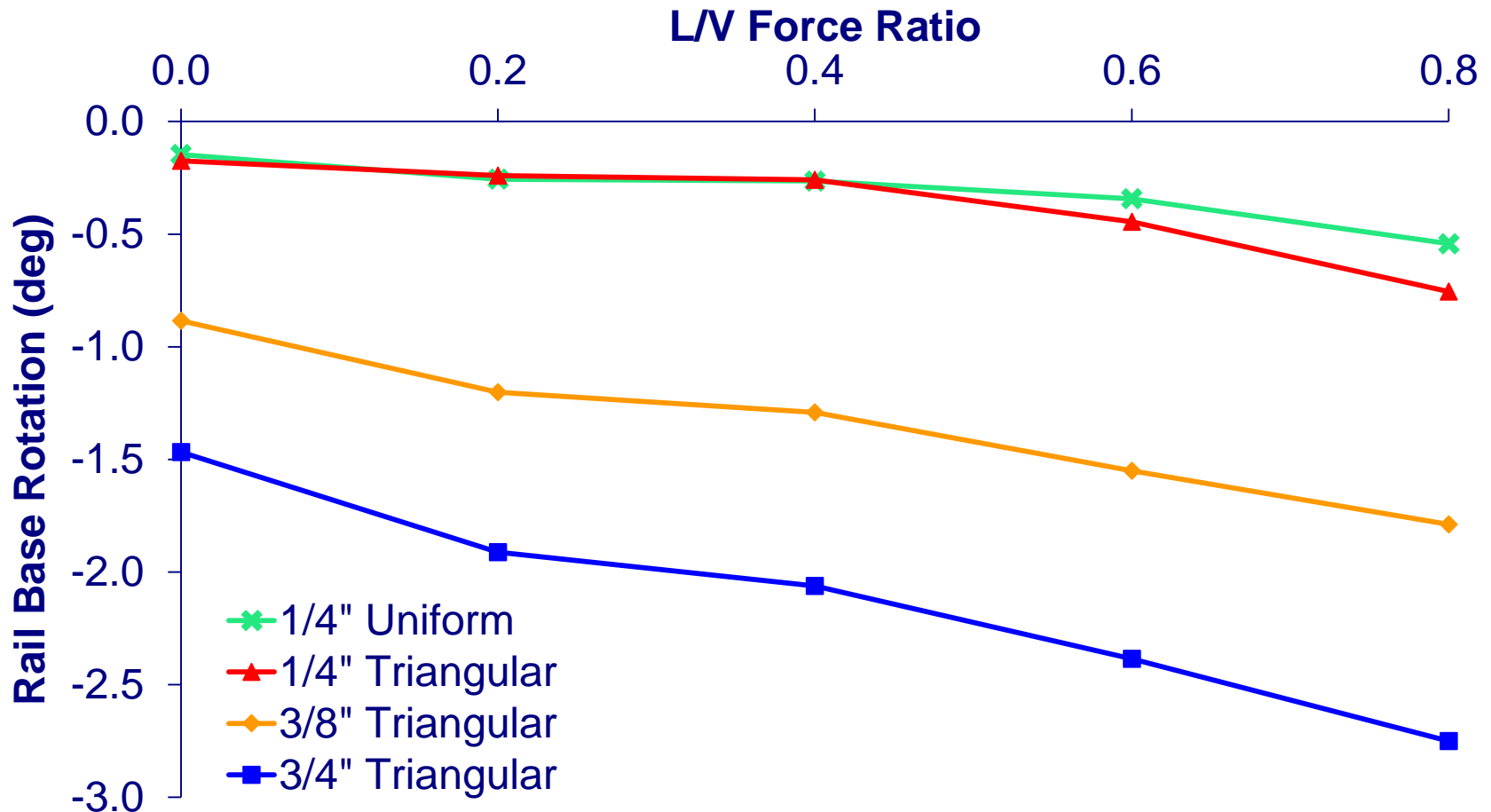
Gauge





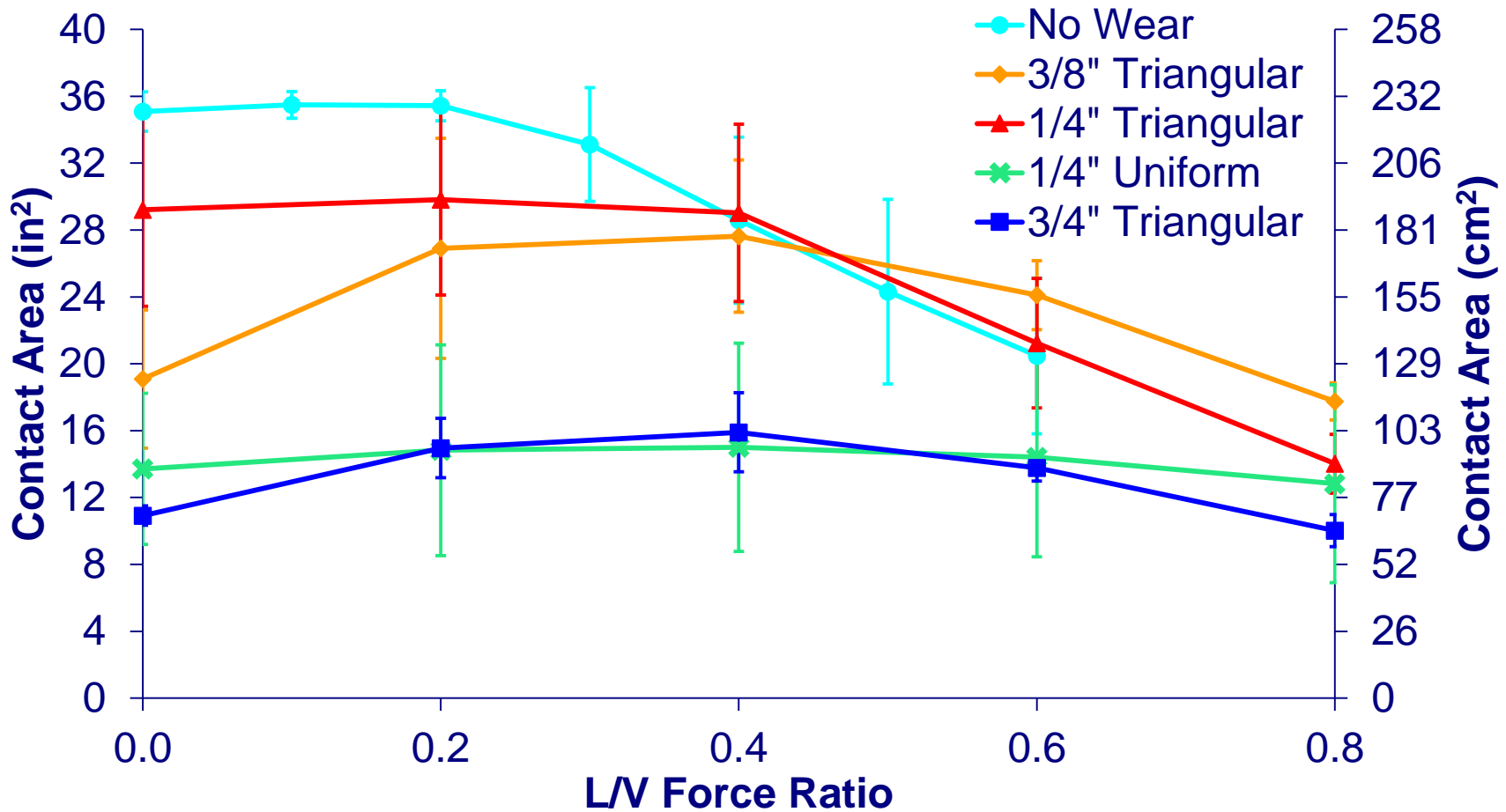
# Effect of L/V Force Ratio on Rail Base Rotation

20,000 lb (88.9 kN) Vertical Wheel Load



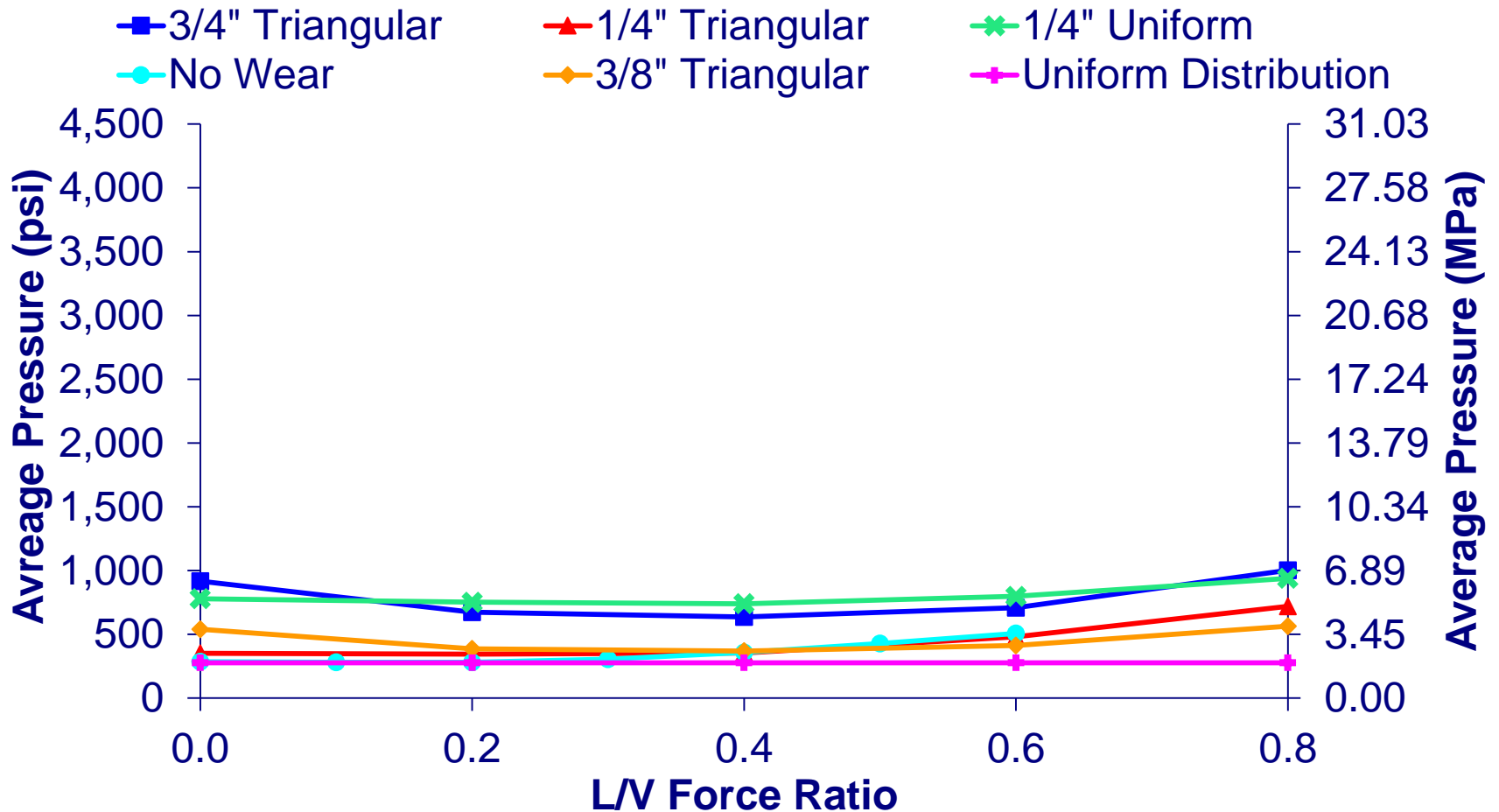
# Loss of Contact Area

20,000 lb (88.9 kN) Vertical Wheel Load



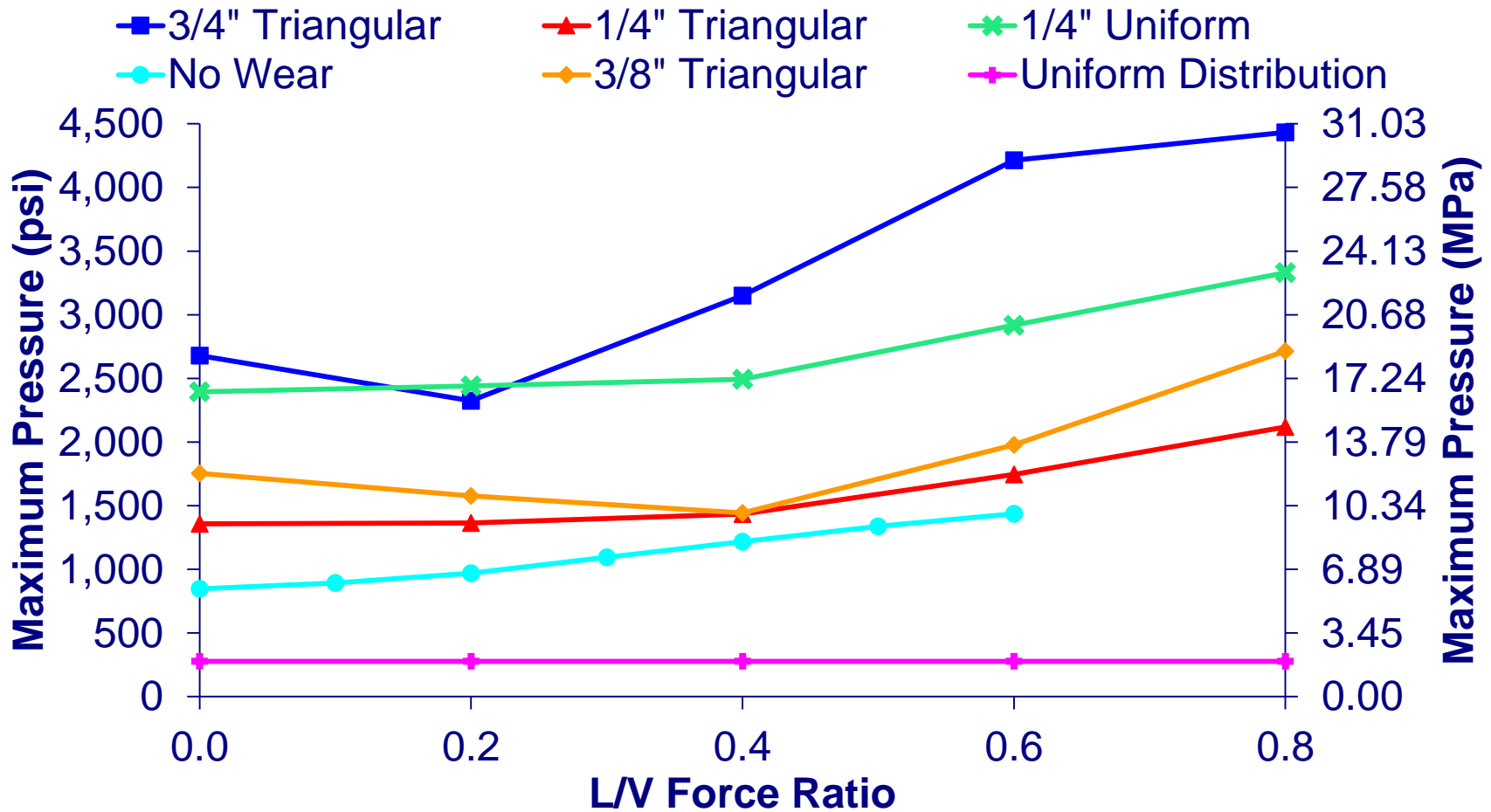
# Effect of Wear Depth on Average Pressure

20,000 lb (88.9 kN) Vertical Wheel Load



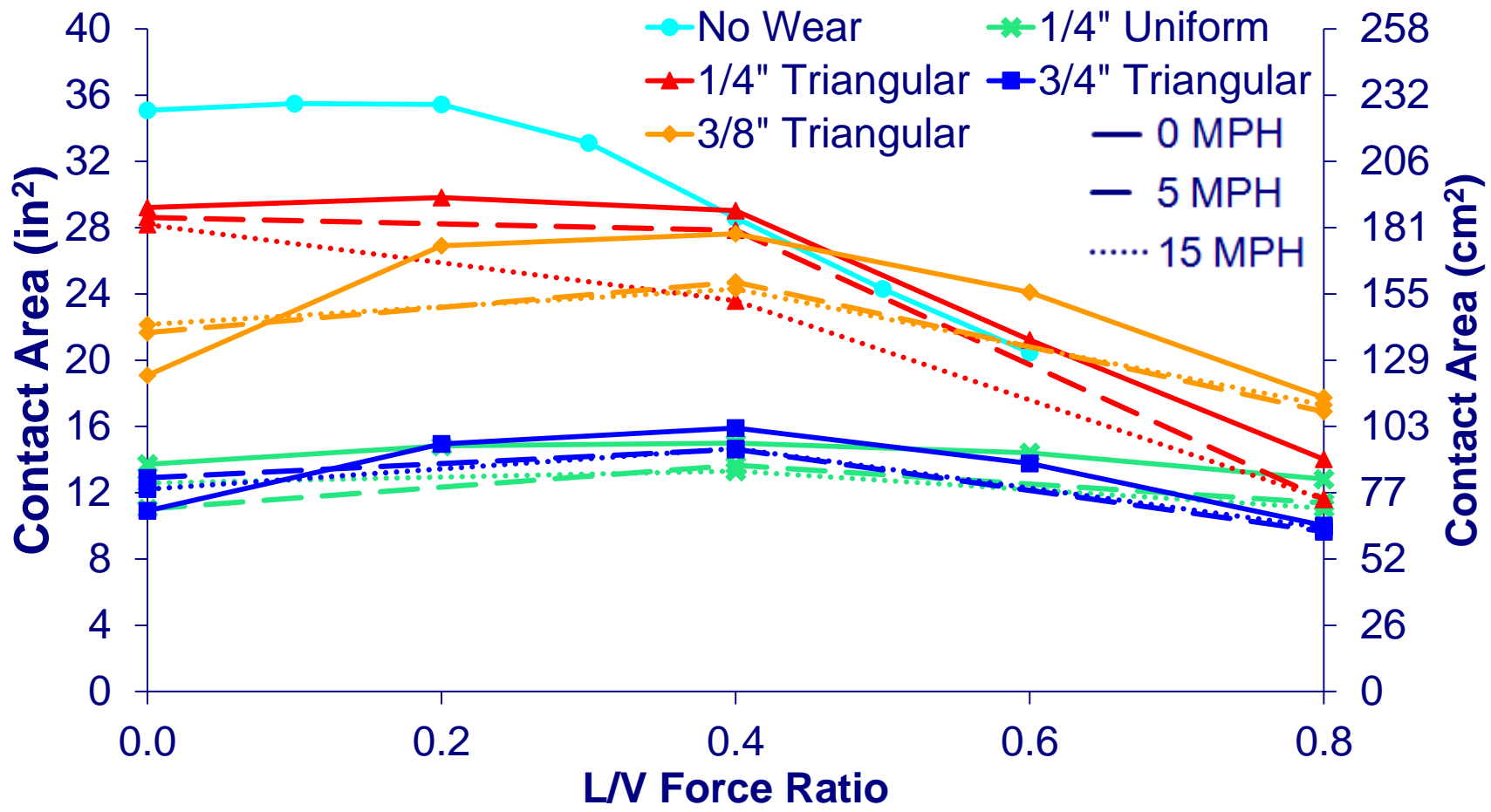
# Effect of Wear Depth on Maximum Pressure

20,000 lb (88.9 kN) Vertical Wheel Load



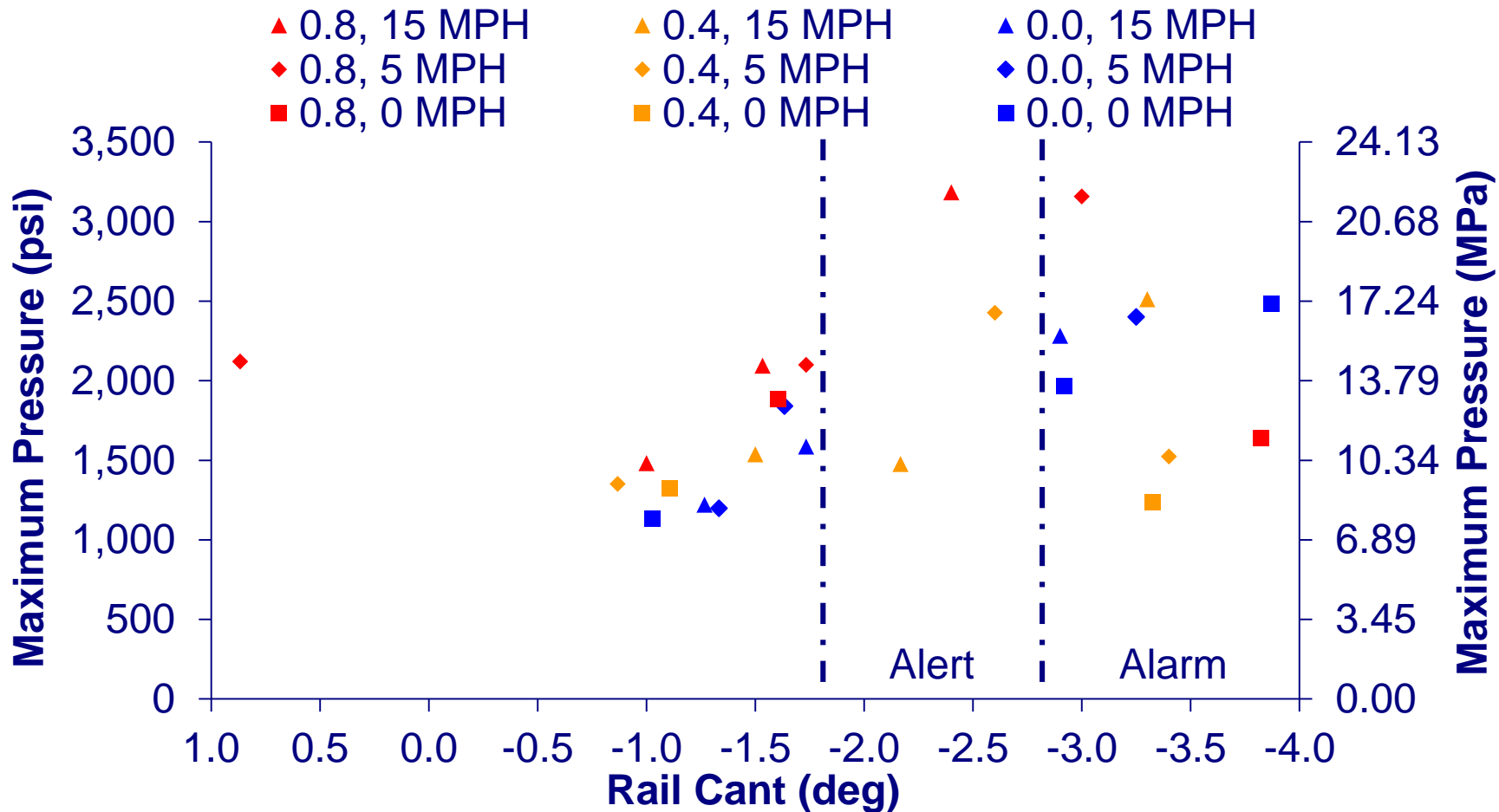
# Effect of Speed on Contact Area

20,000 lb (88.9 kN) Vertical Wheel Load



# Relationship between Rail Cant and Maximum Pressure

20,000 lb (88.9 kN) Vertical Wheel Load





# Conclusions

- Response of rail base rotation to increased L/V force ratios is consistent
  - Magnitude increases with wear depth
- Contact area is reduced by increasing wear depth
  - 75% reduction with doubling of wear depth
  - Loss of contact area increases pressures
    - 16% increase in average pressure (3/4" triangular wear)
    - 65% increase in maximum pressure (3/4" triangular wear)
- At low speeds, train speed has little effect on loading environment
  - 5% average contact area reduction
- Extreme rail seat pressures may be related to excessive rail cant
  - Increased variability with decreased rail cant

# Future Work

- How accurately does artificially-worn RSD replicate field-worn RSD?
- How does the presence of fines or rail seat debris affect RSD failure mechanisms?
- How can these findings be applied to current and proposed industry practice?
  - Can load nonuniformity be correlated to RSD or specific RSD mechanisms?



# Acknowledgements



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